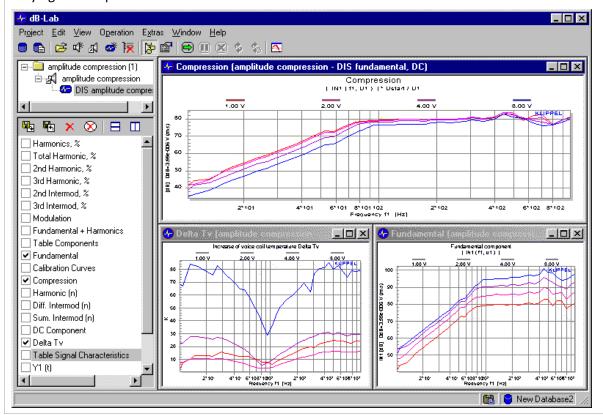
## Causes for Amplitude Compression

Application Note to the KLIPPEL R&D SYSTEM (Document Revision 1.2)

#### **DESCRIPTION**

Both thermal and nonlinear effects limit the amplitude of the fundamental component in the state variables and in the sound pressure output. The 3D distortion module (DIS) module of the Klippel R&D System is used to separate the effects from voice coil heating and from nonlinear parameters varying with displacement.



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## 1 Causes for Amplitude compression

Amplitude Compression	Thermal and nonlinear effects limit the output signal in the large signal domain. Thus the amplitude of the fundamental component in the output signal (e.g. displacement) grows not proportionally with the amplitude of the electrical input signal (e.g. voltage at the speaker terminals).
	The 3D Distortion measurement (DIS) performs a series of measurements with varied voltage $U_1$ of the input signal (amplitude sweep). The result window <i>Compression</i> in the DIS module presents the amplitude of the fundamental by
	$L_C(U_1, f_1) = 20 \lg \left( \frac{P(U_1, f_1)U_{start}}{P_{ref}U_1} \right) = L(U_{start}, f_1) - C(U_1, f_1)$
	while compensating the increase of the input signal. The amplitude compression of the amplitude of fundamental component in the measured signal is defined by
	$C(U_1, f_1) = 20 \lg \left( \frac{P(U_{start}, f_1)U_1}{P(U_1, f_1)U_{start}} \right) = L_C(U_{start}, f_1) - L_C(U_1, f_1)$
	where $U_{\text{start}}$ is the starting value of the amplitude sweep applied to $U_1$ .
Heating of the Coil	The heating of the voice coil and the increase of the voice coil resistance $R_e(T_v)$ is a function of the real electric input power supplied to the speaker and the convection cooling depending on the movement of the coil. Clearly at the resonance where the input impedance is maximal the heating of the coil is minimal.
Nonlinearities	The second source of amplitude compression of the fundamental component are the dominant nonlinearities of the driver such as force factor $Bl(x)$ , inductance $L_e(x)$ and compliance $C_{ms}(x)$ varying with displacement $x$ . At low frequencies where the amplitude of the displacement is high these mechanisms produce the highest compression.
Separating the two effects	The driver is excited by a sinusoidal tone varied in frequency and amplitude. The power compression is measured both in the sound pressure output and in the input current i. Whereas the amplitude compression $C_p(f)$ in the sound pressure reflects both heating and nonlinear effects, the amplitude compression $C_i(f)$ in the current is mainly caused by the heating for frequencies $f$ below and above the resonance frequency $f_s$ .
	Thus the thermal power compression at low and high frequencies is
	$C_{thermal}(U_1, f_1) = C_i(U_1, f_1)$
	and the power compression due to nonlinear effects is
	$C_{nonlinear}(U_1, f_1) = C_p(U_1, f_1) - C_i(U_1, f_1)$
	at low frequencies ( $f_1 < f_s$ ) and high frequencies ( $f_1 > f_s$ ), and
	$C_{nonlinear}(U_1, f_1) = C_p(U_1, f_1)$
	for $f_1=f_s$ .

#### 2 Method of Measurement

Excitation Signal	A sinusoidal signal with variable frequency and amplitude shall be connected to the terminals of the loudspeaker.
	Amplitude Sweep:
	A series of measurements is performed while varying the amplitude in $n_U$ points spaced linearly or logarithmically between starting amplitude $U_{\text{start}}$ and end amplitude $U_{\text{end}}$ .
	Frequency Sweep:
	A series of measurements is performed while varying the frequency in $n_f$ points spaced linearly or logarithmically between starting frequency $f_{\text{start}}$ and end frequency $f_{\text{end.}}$
	For example:
	$U_{start} = 0.1 \text{ V rms}$ , $U_{end} = 2 \text{ V rms}$ (4 points linear spaced) $f_{start} = 20 \text{ Hz}$ , $f_{end} = 1 \text{ kHz}$ (50 points linearly spaced)
Loudspeaker Setup	The loudspeaker shall be brought under free-field or half-space free-field condition. The sound pressure is measured in the near field of the driver or taken in 1 meter from the speaker (on axis).

## 3 Using 3D Distortion Measurement (DIS)

Requirements	<ul> <li>The following hardware and software is required for assessing X<sub>max</sub></li> <li>Distortion Analyzer + PC</li> <li>Software module 3D Distortion Measurement (DIS) + dB-Lab</li> <li>Microphone</li> </ul>
Setup  Don't forget ear protection!	<ul> <li>Connect the microphone to the input IN1 at the rear side of the DA.</li> <li>Set the speaker in the approved environment and connect the terminals with SPEAKER 1.</li> <li>Switch the power amplifier between OUT1 and connector AMPLIFIER.</li> </ul>
Preparation	<ul> <li>Create a new object DRIVER</li> <li>Assign an operation "DIS Amplitude Compression AN12"</li> </ul>
Measurement	<ol> <li>Start the measurement "DIS Amplitude Compression AN12"</li> <li>Select the Signal at IN1 as State signal on property page Display and read the power compression C<sub>p</sub>(U<sub>1</sub>, f<sub>1</sub>) at voltage U<sub>1</sub> and frequency f<sub>1</sub> of interest. Calculate the nonlinear amplitude compression C<sub>nonlinear</sub>.</li> <li>Select the Current Speaker 1 as State signal on property page Display and read the power compression C<sub>i</sub>(U<sub>1</sub>, f<sub>1</sub>) at voltage U<sub>1</sub> and frequency f<sub>1</sub> of interest. Assign the power compression C<sub>i</sub>(U<sub>1</sub>, f<sub>1</sub>) for low frequencies f<sub>1</sub> &lt; f<sub>s</sub> and for high frequencies f<sub>1</sub> &gt; f<sub>s</sub> to the thermal power compression C<sub>thermal</sub>(U<sub>1</sub>, f<sub>1</sub>).</li> </ol>
	4) Print the compression curves or create a report

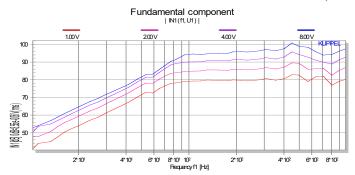
### 4 Setup Parameters for DIS Module

Template	Create a new Object, using the operation template <i>DIS Amplitude Compression AN12</i> in dB-Lab. If this database is not available you may generate DIS 3D Harmonic measurements based on the general DIS module. You may also modify the setup parameters according to your needs.
Default Setting for Harmonic Measurement	<ol> <li>Open the property page Stimulus.         Select mode Harmonics.         Switch on Voltage U<sub>1</sub> Sweep, and set U<sub>start</sub> to 1 V rms and U<sub>end</sub> to 8 V rms measured in 7 points varied linearly. Make sure the signal level is appropriate for loudspeaker.         Switch on the Frequency Sweep with 50 points spaced logarithmically between 20 Hz and 1000 kHz. Set additional excitation time to 0.01 s.</li>         Set maximal order of distortion analysis N = 16. </ol>
	<ol> <li>Open property page <i>Input</i>. Select <i>Mic IN 1</i> at the first channel (Y1). Select <i>Is Current speaker 1</i> on the second channel (Y2).</li> <li>On the <i>Protection</i> property page, enable temperature measurement and set maximal increase of voice coil temperature to 100 K.</li> <li>Open the <i>Display</i> property page. Select <i>Signal at IN1</i> as State signal and. <i>2D plot, versus f1</i>.</li> </ol>

#### 5 Example

# Fundamental sound pressure response

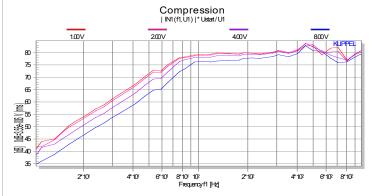
After selecting *Signal at IN1* as State signal on property page *Display* the result window *Fundamental* shows the SPL of the fundamental versus frequency  $f_1$  and amplitude  $U_1$ .



Due to the logarithmic spacing of the input voltage the amplitude responses in SPL are equally spaced in the small signal domain.

# Compression of fundamental

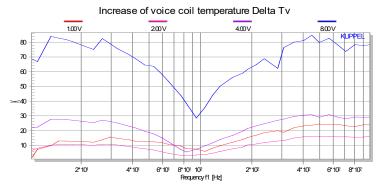
The result window *Compression* shows the SPL of the fundamental referred to the response measured at the starting amplitude  $U_{\text{start}}$ .



The output amplitude is reduced by  $C_p = 7$  dB at low frequencies ( $f_1 < f_s$ ),  $C_p = 5$  dB at the resonance frequency  $f_s$  and about  $C_p = 2$  dB at high amplitude ( $f_1 > f_s$ ), compared by the output of a linear system. Since the heating of the coil is much lower at the resonance frequency the nonlinear compression  $C_{nonlinear}(f_s) \approx C_p(f_s)$ .

#### Voice Coil Temperature

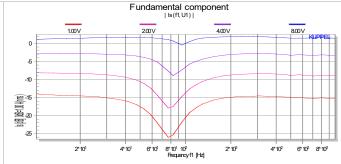
The result window *Delta Tv* shows the increase of the voice coil temperature  $dT_v$  in Kelvin measured after each point of the amplitude and frequency sweep.



The heating of the coil is maximal at low and high frequencies and maximal amplitude. There is a distinct minimum of the voice coil temperature at resonance frequency.

#### Current Fundamental

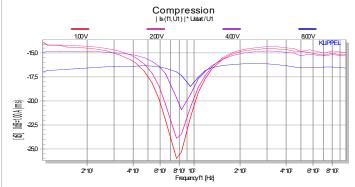
After selecting the *Current Speaker 1* as displayed signal on property page *Display* the results window *Fundamental* shows the amplitude response of the fundamental component.



In the small signal domain the responses are equally spaced according to variation of the terminal voltage  $U_1$ . The distinct minimum shows the resonance frequency  $f_s$  rising from 75 Hz to 95 Hz with amplitude. The shape of the response also changes dramatically due to variation of stiffness  $K_{ms}(x)$  and electrical loss factor  $Q_{es}(x)$  with the displacement x.

# Thermal power Compression

The result window *Compression* shows the fundamental of input current referred to the response at the starting amplitude U<sub>start</sub>.



The amplitude of the current is reduced by  $C_i=3$  dB at low frequencies  $(f_1 < f_s)$  compared by the output of a linear system. This is mainly caused by thermal power compression  $C_{thermal}=C_i$ . In comparison to the compression in sound pressure of  $C_p\approx 7$  dB the nonlinear compression is about  $C_{nonlinear}=C_p-C_i\approx 4$  dB. At high frequencies  $(f_s < f_1)$  the thermal power compression is about  $C_{thermal}=C_i\approx 2$  dB.

#### 6 More Information

Related Specification	S4_DIS
Papers	W. Klippel, "Loudspeaker Nonlinearities – Causes, Parameters, Symptoms" preprint #6584 presented at the 119 <sup>th</sup> Convention of the Audio Engineering Society, 2006 October 6-8, San Francisco, USA Updated version on http://www.klippel.de/know-how/literature/papers.html
Software	User Manual for the KLIPPEL R&D SYSTEM

Find explanations for symbols at:

http://www.klippel.de/know-how/literature.html

Last updated: 9.2.16

